

Introduction to ANSYS CFX

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Introduction ANSYS®

- **Lecture Theme:**
	- **Heat transfer has broad applications across all industries. All modes of heat transfer (conduction, convection – forced and natural, radiation, phase change) can be modeled.**
- **Learning Aims:**
	- **You will be familiar with CFX's heat transfer modeling capabilities and be able to set up and solve problems involving all modes of heat transfer**

Mechanisms ANSYS®

- **Convection**
	- **Heat transfer due to the bulk movement of a fluid**
	- **Forced: flow is induced by some external means**
	- **Natural or Free: fluid moves due to buoyancy effects**
	- **Boiling: phase change (not covered in this course)**

- **Conduction**
	- **Heat transfer in a fluid or solid due to differences in temperature**
	- **Conduction is described by Fourier's law:**
		- **heat flux is directly proportional to the negative temperature gradient**

- **Radiation**
	- **Transfer of thermal energy by electromagnetic waves from 0.1 µm (ultraviolet) to 100 µm (mid-infrared)**
	- **Radiation intensity is directionally and spatially dependent**
- **Viscous Dissipation**
	- **Energy source due to viscous heating**
	- **Important when viscous shear in fluid is large (e.g., lubrication) and/or in high-velocity, compressible flows**

 log_{10} (Wavelength), μ m

Heat Transfer Models: Fluid Domains ANSYS®

- **Heat Transfer option**
	- **None:**
		- **Energy Transport not solved**
	- **Isothermal:**
		- **Energy Transport not solved, temperature is set for the evaluation of fluid properties**
	- **Thermal Energy:**
		- **Energy Transport is solved; kinetic energy effects neglected**
		- **For low speed flow**
	- **Total Energy:**
		- **Transport of enthalpy and kinetic energy effects**
		- **For Mach number > 0.3 or compressibility effects,**
		- **For low speed liquid flow when the specific heat is not constant**

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Mechanisms > Energy Equation Models > Wall BCs > CHT > Post > Tips/Summary

Heat Transfer Models: Fluid Domains ANSYS®

- **If natural convection is important, then switch on the Buoyancy Model**
	- **For varying density full buoyancy model used**
	- **For constant density Boussinesq model used**
- **Thermal Radiation model**
	- **Should be accounted for when**

$$
Q_{rad} = \sigma \left(T_{\text{max}}^4 - T_{\text{min}}^4 \right) \ge Q_{conv} = h \left(T_{wall} - T_{free} \right)
$$

• **Several radiation models are available which provide approximate solutions to the RTE (more information in appendix)**

Governing Equation : Solid domains ANSYS®

• **Heat transfer in a solid domain is modeled using the following conduction equation:**

$$
\frac{\partial(\rho h)}{\partial t} + \nabla \cdot (\rho U_s h) = \nabla \cdot (\lambda \nabla T) + S_E
$$
\nTransient Solid motion Conduction Source

Mechanisms Energy Equation Models Wall BCs CHT > Post Tips/Summary

• **h is the sensible enthalpy :**

$$
h = \int_{T_{ref}}^{T} c_p dT
$$

Heat Transfer Models: Solid Domains ANSYS®

- **For conduction set Heat Transfer option to Thermal Energy**
- **Thermal radiation in solids**
	- **Required only for transparent or semi-transparent materials, e.g. glass; no radiation in opaque solids**
	- **Monte Carlo model only**

Details of Domain 1 in Flow Analysis 1

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Thermal Wall Boundary Condition

- **Thermal boundary conditions come in three types, all available in ANSYS CFX:**
	- **Neumann**
	- **Robin/Fourier**
	- **Dirichlet**
- **They represent heat transfer phenomena outside the domain**

Conjugate Heat Transfer (CHT) - Domain Interfaces

- **GGI connection is only option for Fluid-Solid and Solid-Solid interfaces because…**
	- **GGI interface**
		- **No discontinuity in values of temperature across the interface**
		- **CFX Solver calculates a "surface temperature" based on a fluxconservation equation**
	- **1:1 interface**
		- **May result in temperature discontinuity at the interface**
- **Radiation conditions are set on the side in which radiation is modelled, e.g. the fluid side of a fluid/solid interface**

Conjugate Heat Transfer – Modelling Walls ANSYS®

Wall thickness meshed:

• **Fourier's Law Solved in 3D**

- **Energy equation solved in solid**
- **Accurate approach requires more meshing & computational effort**

Wall thickness NOT meshed (thin wall):

• **1-D Fourier's Law through Wall**

- **Artificially models conduction across wall thickness**
- **Limitation: conduction is assumed to be normal to the wall**

Conjugate Heat Transfer – Thin walls ANSYS®

- **Set-up**
	- **Create a Fluid-Fluid Domain Interface**
	- **On Additional Interface Models tab set Mass and Momentum = No Slip Wall**

Mechanisms \sum Energy Equation Models \sum Wall BCs

- **Enable Heat Transfer toggle and pick:**
	- **Thin Material and specify a Material & Thickness or Thermal Contact Resistance**
	- **Note : Other domain interface types (Fluid-Solid etc.) can use these options to represent coatings etc.**

Post-Processing Heat Transfer ANSYS®

- **Temperature:**
	- **Local fluid temperature, plotted on a wall it is the temperature at the wall, Twall**
- **Wall Adjacent Temperature:**
	- **Average temperature in control volume next to wall**
- Wall Heat Transfer Coefficient, h_c:
	- **Based on Twall and the Wall Adjacent Temperature by default**
	- **To base it on some far-field value instead of the Wall Adjacent Temperature, use the Expert Parameter "tbulk for htc"**
- **Wall Heat Flux, qw:**
	- **Total heat flux into the domain by all modes**
	- **Available on all boundaries**

*T*_{wall} *q*_{*w*} Mesh Control Volumes

 $q_w = h_c (T_{wall} - T_{ref})$

Where *Tref* is the *Wall Adjacent Temperature* or the *tbulk for htc* temperature if specified

Post-Processing Heat Transfer ANSYS

- **Heat Flux:**
	- **Total convective and radiative heat flux into the domain**
	- **Available on all boundaries**
	- **On flow boundaries, it represents the energy carried with the fluid relative to its Reference Temperature**
- **Wall Radiative Heat Flux:**
	- **Net radiative energy leaving the boundary**
	- **Wall Convective Heat Flux + Wall Radiative Heat Flux = Wall Heat Flux**
	- **Only applicable when radiation is modeled**
- **Wall Irradiation Flux:**
	- **Incoming radiative flux**
	- **Only applicable when radiation is modeled**

Solution Convergence ANSYS®

- **Allow sufficient solution time**
	- **Heat imbalances in all domains have to approach zero**
- **Monitor**
	- **Create Solver Monitors showing IMBALANCE levels for fluid and solid domains**
	- **View the imbalance information printed at the end of the solver output file**
	- **Use a Conservation Target when defining Solver Control in CFX-Pre**

- **When modelling heat transfer, you must provide :**
	- **Thermal conditions at walls and flow boundaries**
	- **Thermal properties for materials**
- **Available heat transfer modeling options include :**
	- **Species diffusion heat source**
	- **Combustion heat source**
	- **Conjugate heat transfer**
	- **Natural convection**
	- **Radiation**
	- **Periodic heat transfer**

Workshop 05 Electronics Cooling ANSYS®

Dissipation of heat from a hot electronics component

- **Conjugate Heat Transfer (CHT)**
- **Two runs**
	- **First run includes convection and conduction**
	- **Second run adds thermal radiation**

The entire calculation takes a long time to run. So results are provided for postprocessing.

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Natural Convection

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• **The significance of natural convection can be assessed through the Richardson number , Ri:** *Forced Natural U* $Ri = \frac{g\beta\Delta TL}{T^2} =$ $=\frac{g\beta\Delta T}{H^2}$ β_{4}

• In buoyancy-driven flows, the Rayleigh number, Ra, indicates the relative importance of

convection and conduction:
 $Ra_x = \frac{g\beta\Delta Tx^3}{V\alpha} = \frac{buoyancy force}{Viscous losses \& thermal\ diffusion}$ **convection and conduction:** 3

$$
Ra_x = \frac{g\beta\Delta Tx^3}{v\alpha} = \frac{buoyancy force}{viscous losses & thermal diffusion}
$$

– **The size of Ra is a measure of whether a natural convection boundary layer is laminar or turbulent. For a vertical surface the critical value is around 10⁹ but the transition zone ranges from 10⁶ to 10⁹ .**

Radiation: Mechanism

• **Transfer of thermal energy by electromagnetic waves from 0.1 µm (ultraviolet) to 100 µm (mid-infrared).**

 log_{10} (Wavelength), μ m

- **Radiation intensity is directionally and spatially dependent**
- **Transport mechanisms for radiation intensity along one given direction:**

– **Scattering occurs when particles are present in the fluid - often neglected.**

Radiation: Choice of Model ANSYS®

- **The optical thickness should be estimated before choosing a radiation model**
	- **The optical thickness τ = a.L**
		- **a is the absorption coefficient (m-1) (Note: ≠ absorptivity of a surface)**
		- **L is the mean beam path length (m)**
		- \cdot **a** = 0.25 to 0.3 m⁻¹ for combustion product gases, = 0.01 m⁻¹ for air and **is proportional to absolute pressure**
		- **L is a typical distance between opposing walls**
- **Optically thin (τ < 1) means that the fluid is partially transparent to thermal radiation**
- **Optically thick (τ > 1) means that the fluid absorbs or scatters the radiation many times before it can interact with the surfaces**

Radiation: Choice of Model ANSYS

- **For optically thick media (τ > 1) the P1 model is a good choice**
	- **Assumes radiative intensity is independent of direction**
	- **The P1 model gives reasonable accuracy without too much computational effort**
- **The Monte Carlo and Discrete Transfer models for any optical thickness**
	- **Both are ray tracing models**
	- **Discrete Transfer is much quicker as it pre-calculates rays in fixed directions but can be less accurate in models with long/thin geometries due to ray effects**
	- **Monte Carlo more expensive to run but recommended for complex geometries and multiband spectral modelling**
- **Surface to Surface Model**
	- **Available for Monte Carlo and Discrete Transfer models**
	- **Neglects the influence of the fluid on the radiation field**
	- **Can significantly reduce the solution time**